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Impact of PWM Resolution in Digital Feedback Loop Precision Power Supplies

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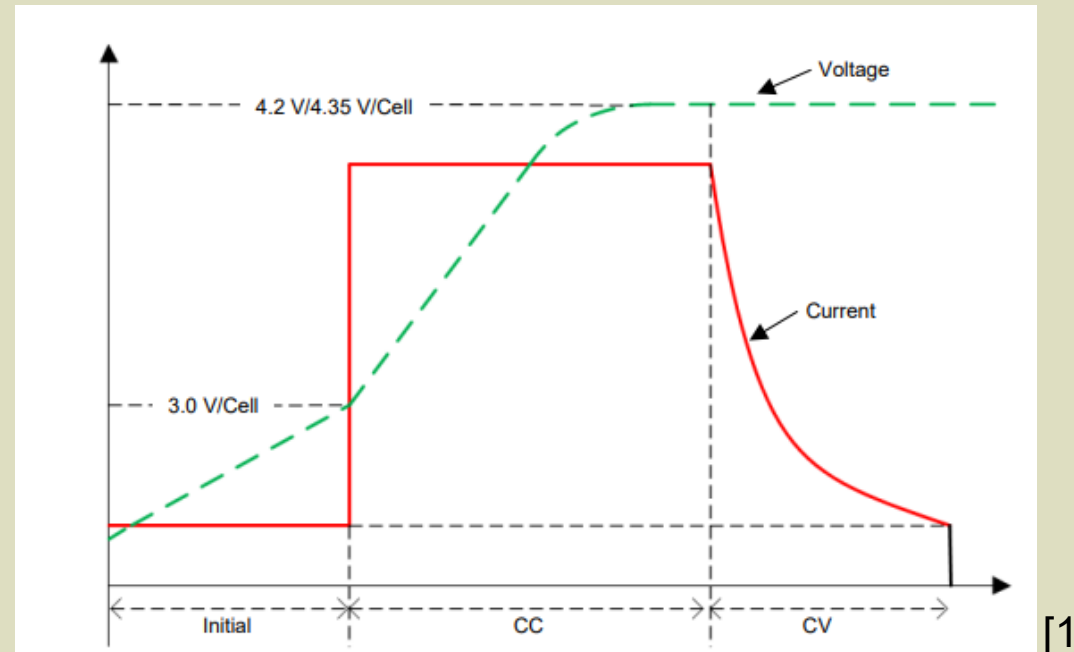


Impact of PWM Resolution in Digital Feedback Loop Precision Power Supplies

2



Forming and Testing Lithium batteries require a precise current and voltage output power supply



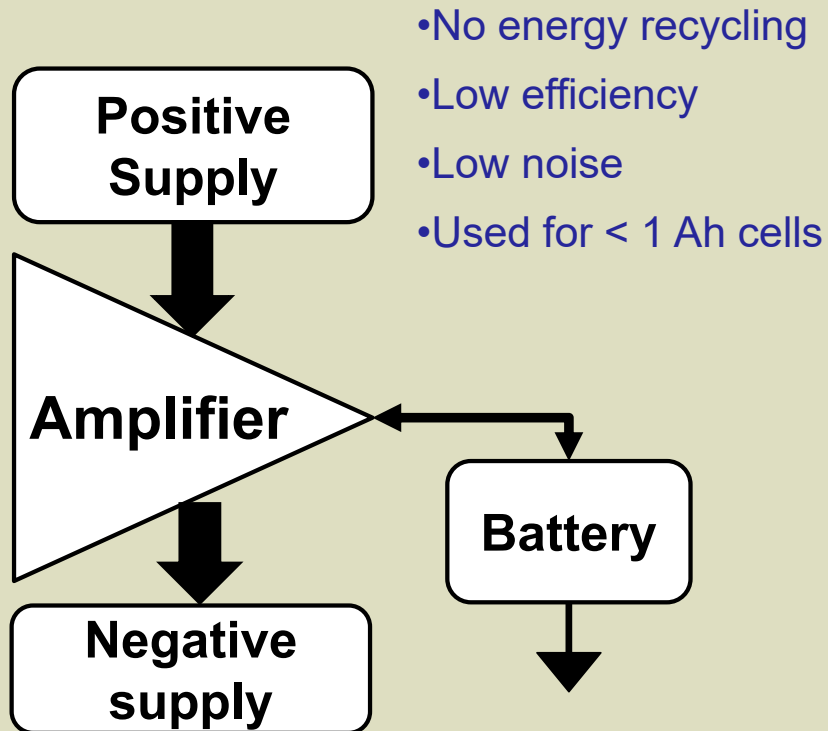
Charging profile of a Li-ion cell

CC: Constant current
CV: Constant voltage

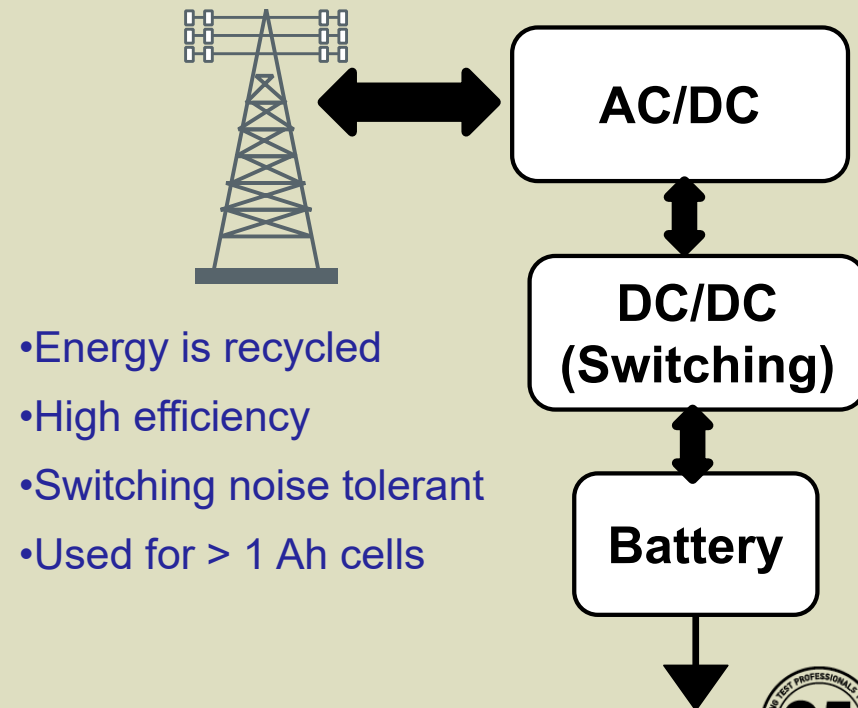


Linear mode DC supply compared to switching mode ^[2]

Linear DC supply (ATE)



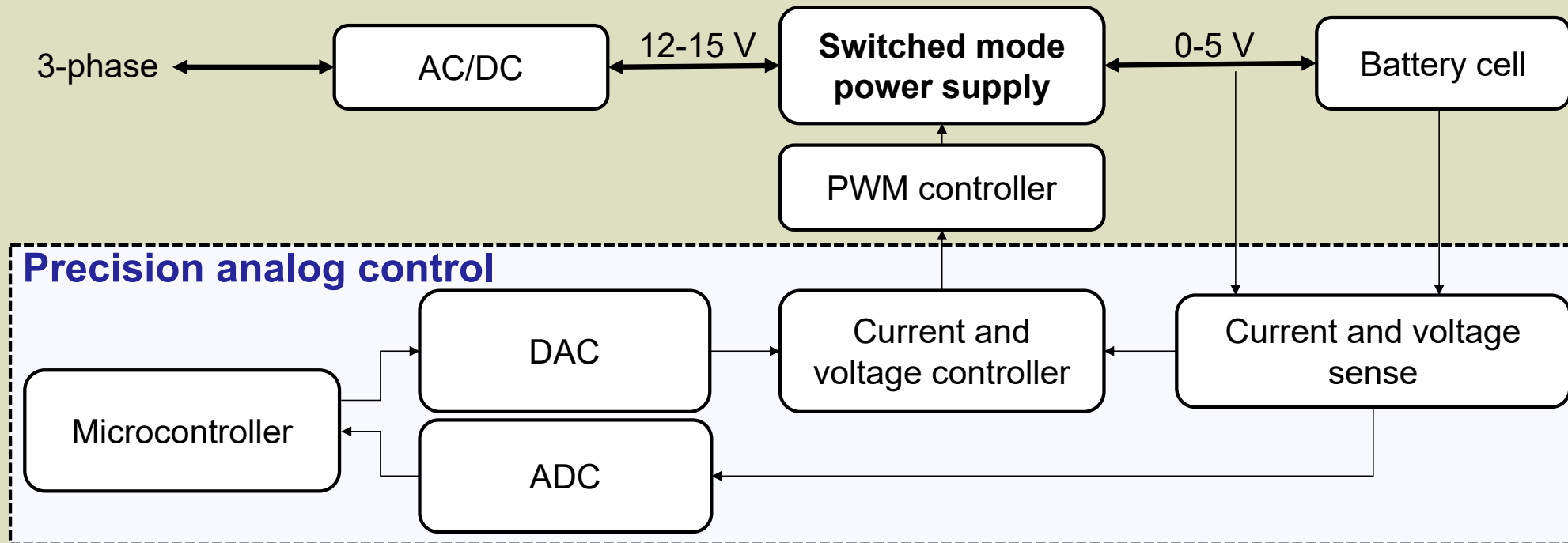
Switched Mode DC supply



Impact of PWM Resolution in Digital Feedback Loop Precision Power Supplies



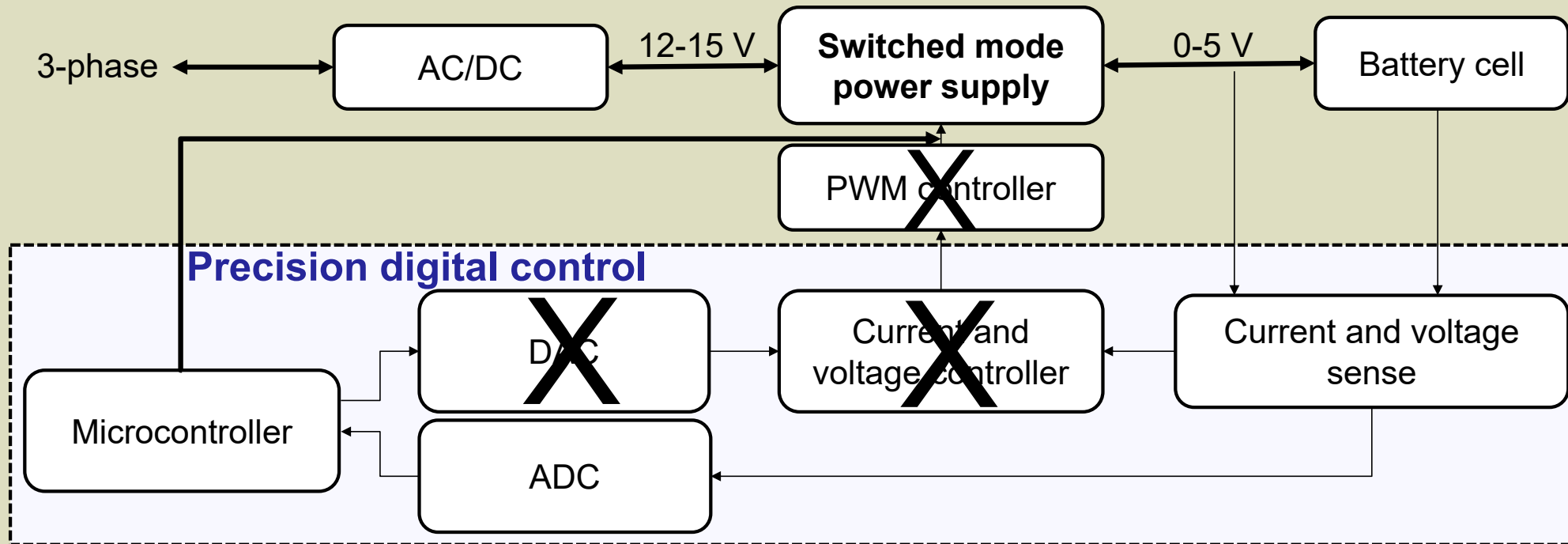
Analog feedback DC power supply [2]



High precision 14-18 bits resolution ADC and DAC are used.

Digital feedback DC power supply [2]

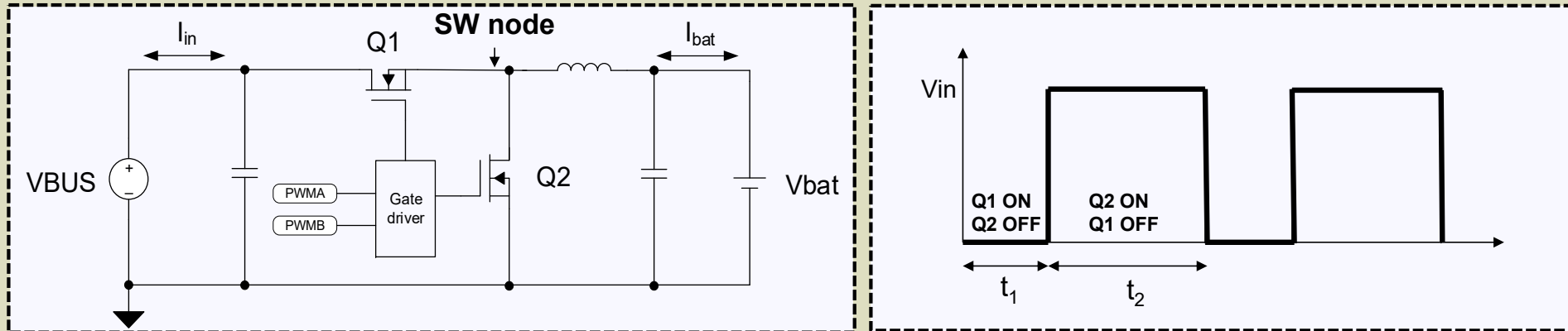
X – Not required



Higher integration and design flexibility with scalable software.



Operating principle of a buck converter



Schematic of a synchronous buck converter

SW node waveform

$$V_{out} = V_{in} * \frac{t_1}{t_1+t_2}$$

$\frac{t_1}{t_1+t_2}$ is called as **duty cycle** of the converter

$\frac{1}{t_1+t_2}$ is **switching frequency** of the converter

Buck converter can be used to control both charging and discharging [4].

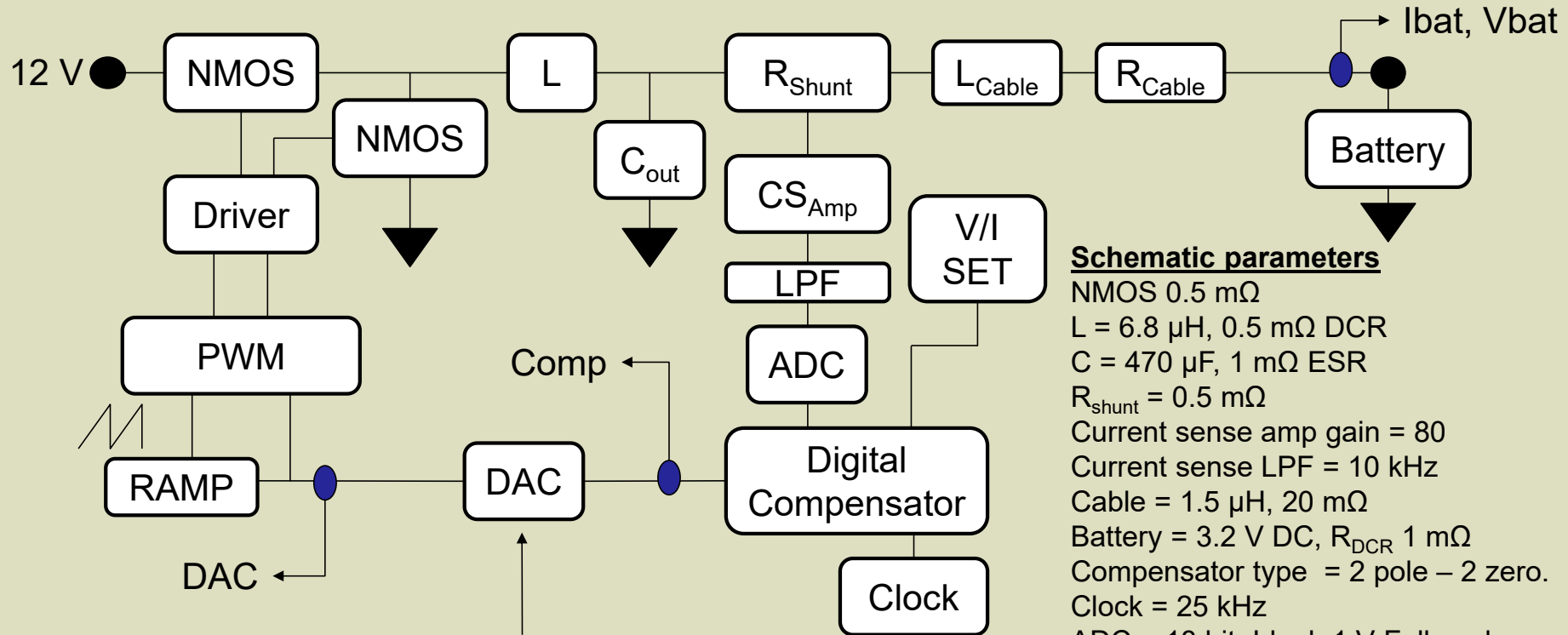
Calculating resolution of PWM signals

Specifications	
Input voltage	12 V
Output voltage	0-5 V
Output current range	-50 A to 50 A
Precision current and voltage control	$\pm 0.01\%$ of full-scale range
Total path resistance (includes inductor, sense resistor, PCB parasitic, cables and internal battery resistance)	20 mΩ (Cable resistance has most impact)
Required output voltage resolution for voltage control	$5\text{ V} \times 0.02\% = 1\text{ mV}$
Required PWM resolution for voltage control	$12\text{ V} / 1\text{ mV} = \sim 13.5\text{ bits}$
Required output voltage resolution for current control	$50\text{ A} \times 20\text{ m}\Omega \times 0.02\% = \mathbf{200\ \mu V}$
Required PWM resolution for current control	$12\text{ V} / 200\ \mu V = \mathbf{\sim 16\text{-bit}}$

16-bit PWM only provides 12-bit precision!



Modeling a Digitally Current Controlled Buck Regulator



Schematic parameters

- NMOS 0.5 mΩ
- L = 6.8 μH, 0.5 mΩ DCR
- C = 470 μF, 1 mΩ ESR
- R_{shunt} = 0.5 mΩ
- Current sense amp gain = 80
- Current sense LPF = 10 kHz
- Cable = 1.5 μH, 20 mΩ
- Battery = 3.2 V DC, R_{DCR} 1 mΩ
- Compensator type = 2 pole – 2 zero.
- Clock = 25 kHz
- ADC = 18 bit, Ideal, 1 V Full-scale
- DAC = 16/14/12-bit, Ideal, 1 V Full-scale
- Ramp = 100 kHz 1 V_{pp}
- Loop bandwidth = 700 Hz

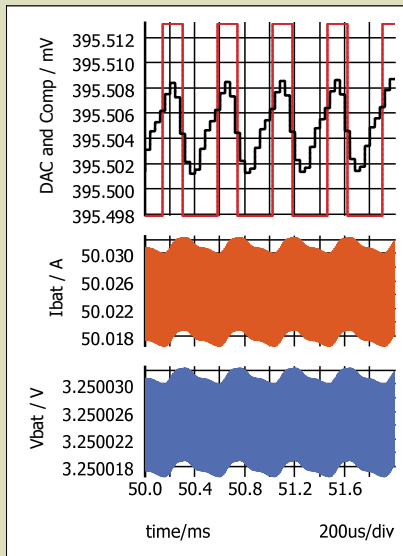
Adjusting resolution of the DAC

Probe



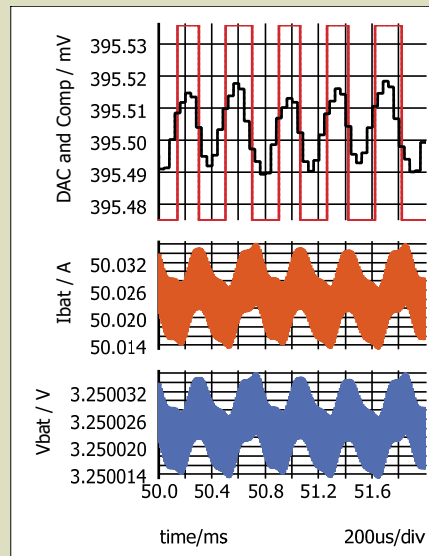
When PWM resolution is not enough!

16-bit PWM



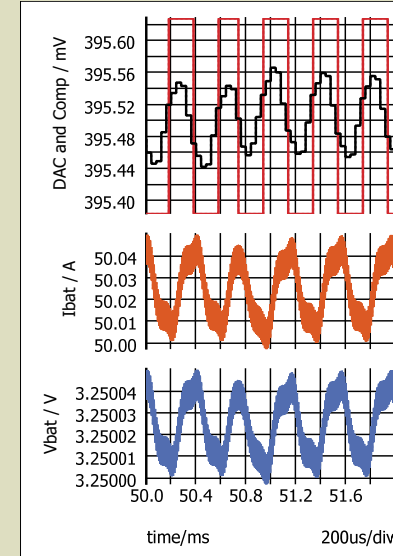
1 LSB of 12 V = 180 μ V

14-bit PWM



1 LSB of 12 V = 0.8 mV

12-bit PWM



1 LSB of 12 V = 3 mV

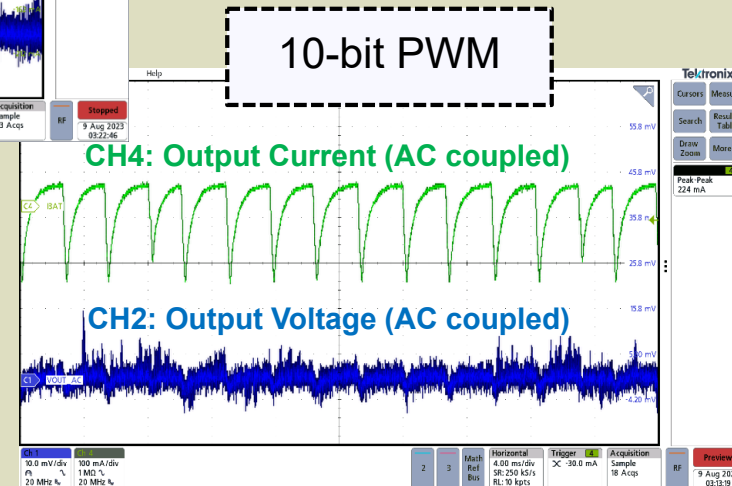
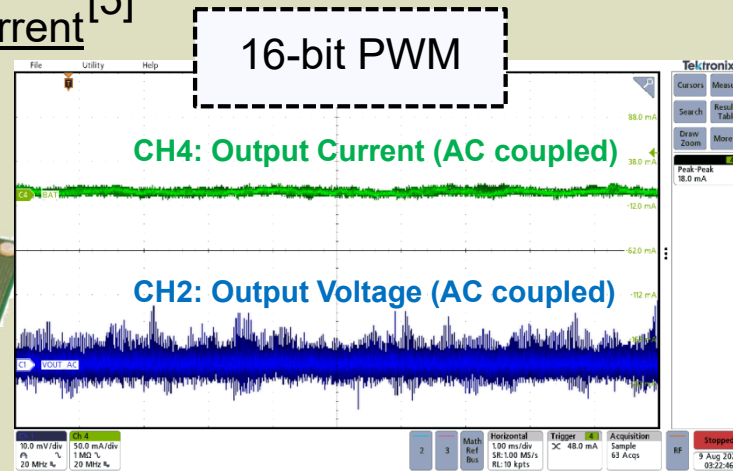
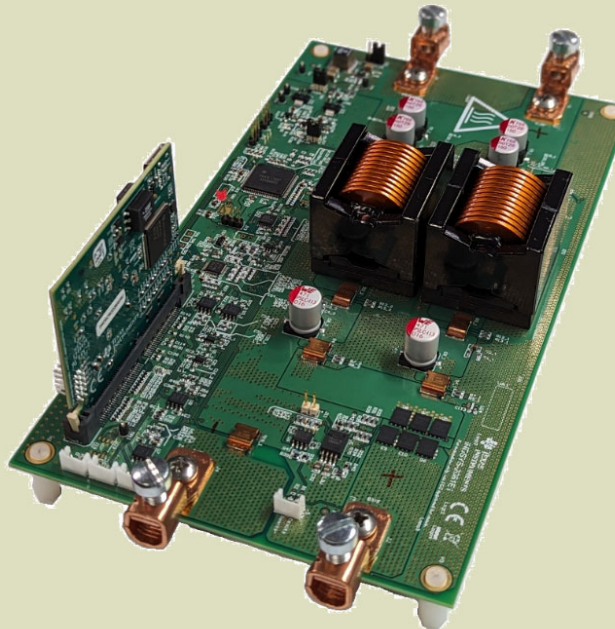
-DAC
-Comp
-Ibat
-Vbat

Low frequency oscillation is seen in the loop bandwidth of the converter.



Validating impact of PWM resolution

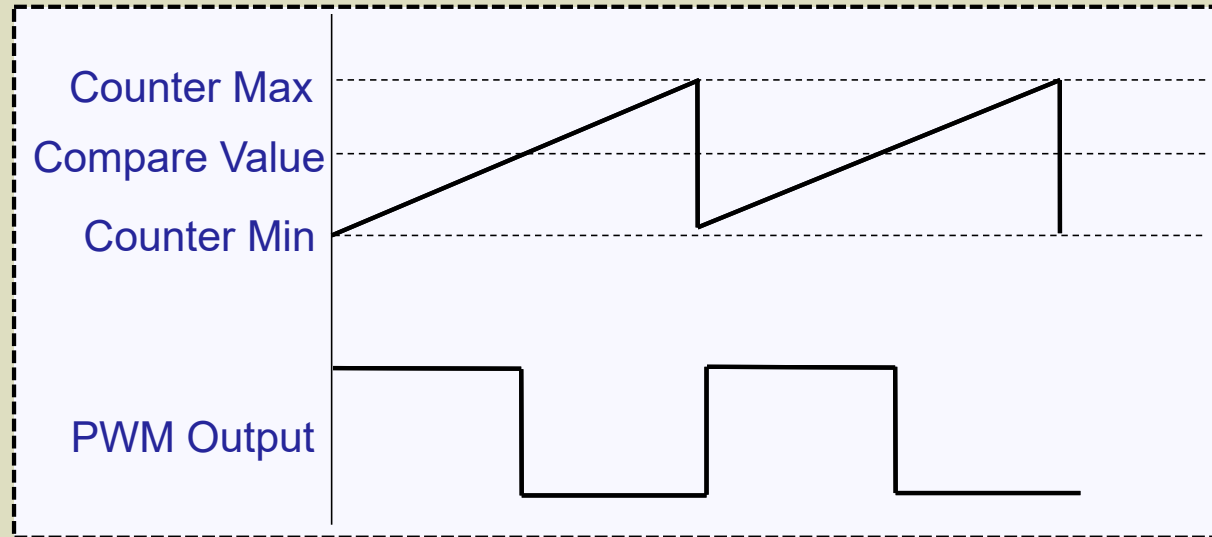
100-A digitally controlled current output buck converter^[5]



Current ripple exceeds 200 mA for 10-bit PWM.



How PWM signals are produced in MCUs?



PWM frequency = 100 kHz (10 μ s)
Digital counter frequency = 100 MHz (10 ns)
Counter steps = 10 μ s / 10 ns = 1000 or ~10-bit

PWM resolution directly depends frequency of the counter.



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PWM Resolution inversely proportional to switching frequency (F_{sw})

10 ns time resolution

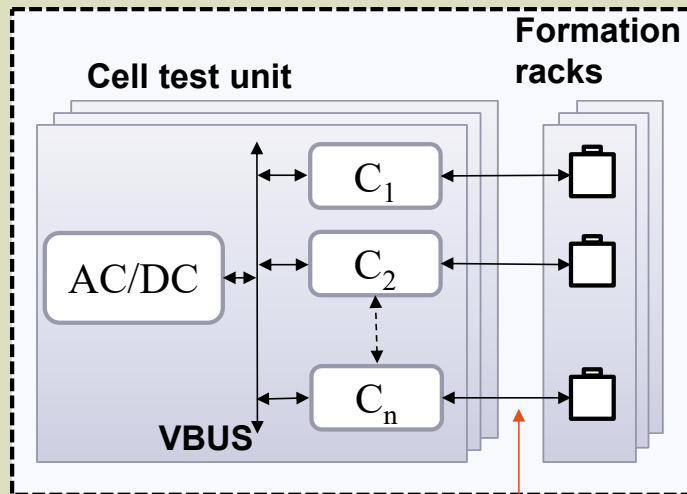
150 ps time resolution

PWM Frequency (kHz)	Regular Resolution (PWM) 100 MHz EPWMCLK		High Resolution (HRPWM)	
	Bits	%	Bits	%
20	12.3	0.02	18.1	0.000
50	11	0.05	16.8	0.001
100	10	0.1	15.8	0.002
150	9.4	0.15	15.2	0.003
200	9	0.2	14.8	0.004
250	8.6	0.25	14.4	0.005
500	7.6	0.5	13.4	0.009
1000	6.6	1	12.4	0.018
1500	6.1	1.5	11.9	0.027
2000	5.6	2	11.4	0.036

Source: TM320F28003x datasheet

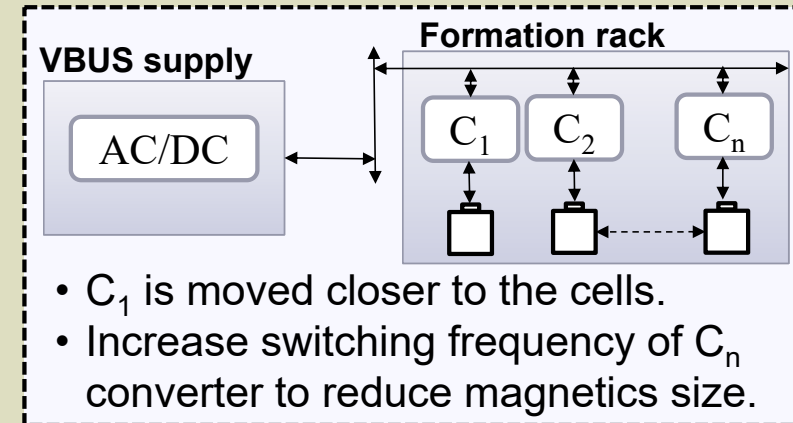
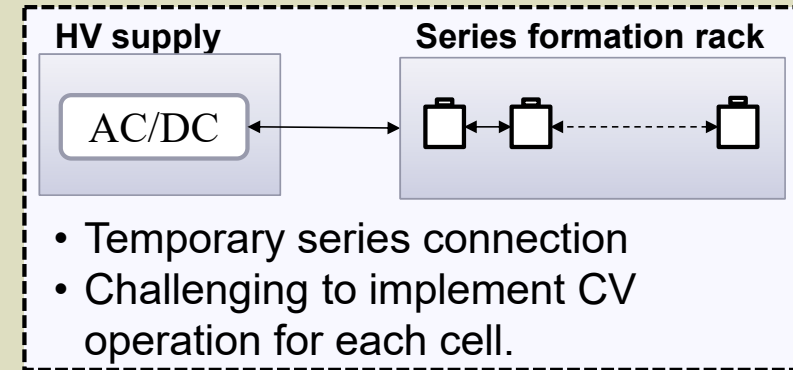


Point-of-load testing requires increase in F_{sw}



Cable optimization

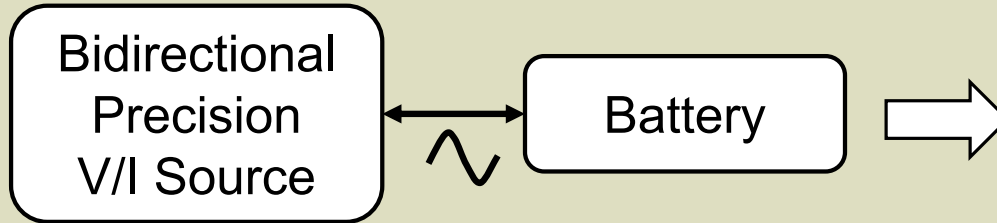
Cable length up to 10 m often reduces power efficiency by about 10%.



C_n : N^{th} test channel, supports CC/CV charge and discharge operation

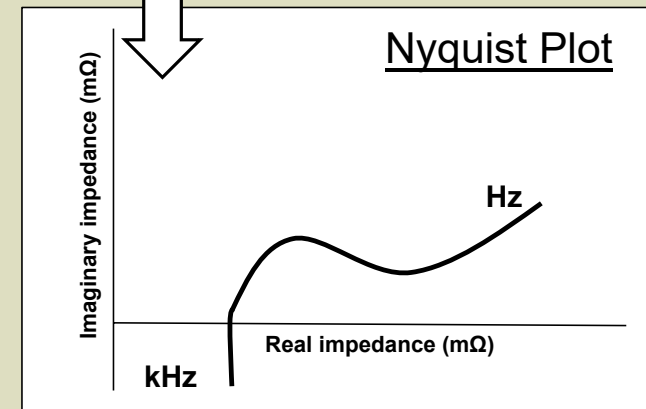
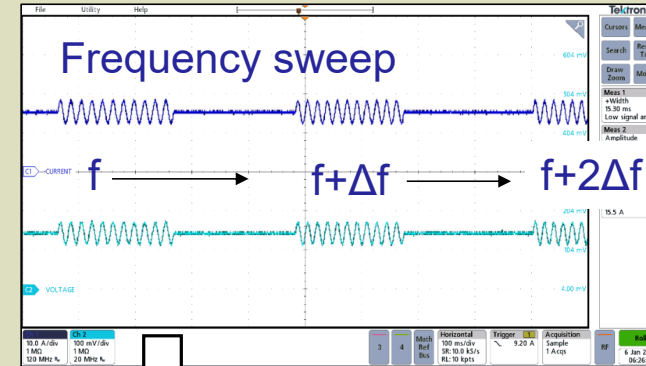


Increase F_{sw} and loop bandwidth for impedance testing



Electrochemical impedance spectroscopy (EIS)

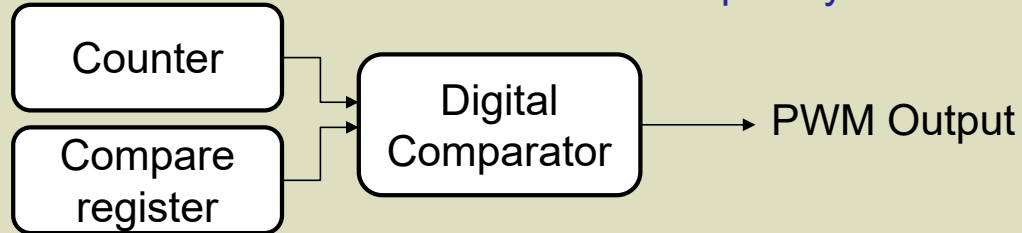
1. Inject sinusoidal current signal
2. Measure battery voltage and current
3. Impedance of cell is $\frac{V \angle \theta_1}{I \angle \theta_2}$
4. Sweep the frequency, and draw Nyquist plot



Comparing methods of PWM generation

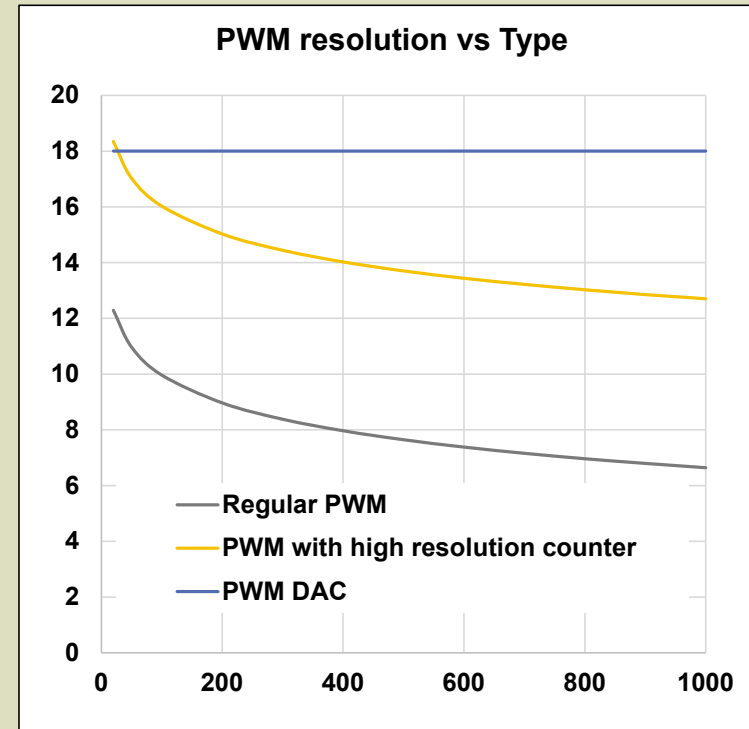
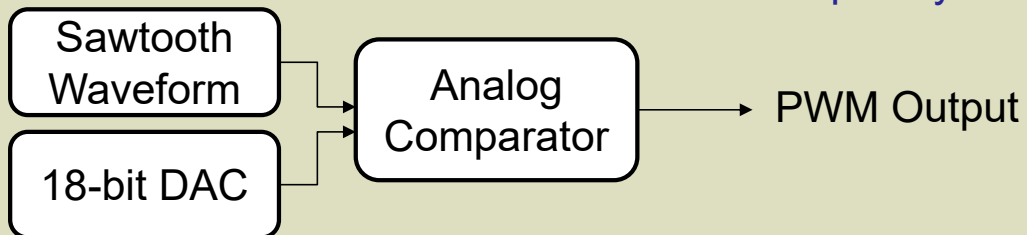
(1) Regular PWM:

Precision suffers with increase in frequency



(2) High Precision PWM DAC

Precision doesn't suffer with increase in frequency



Use a PWM DAC to maximize system performance. Dithering is an alternate method to improve PWM precision. Analysis of dithering is beyond the scope of this paper.



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What we learnt in this presentation

- PWM resolution directly impacts output ripple of the converter.
- Battery instrumentation requires μV resolution for precise charge and discharge control.
- Increasing switching frequency of the power converters reduces power electronics size, which is needed for point-of-load battery formation and testing.
- Higher switching frequency also enables > 10 kHz closed loop bandwidth which allows battery impedance testing.
- Precision of regular PWM outputs of MCUs falls with increase in switching frequency. Regular PWMs cannot be used with wide-band gap semiconductors that has ability to operate at higher switching frequency while delivering more power.
- Precision analog based PWM is needed for power instruments that use wide bandgap semiconductors.



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References

- [1] [Battery Tester Reference Design for High Current Applications User guide, Texas Instruments, 2018](#)
- [2] [Li-ion cell formation and test overview, TestConX, 2023](#)
- [3] [How to design one battery tester for a wide range of sizes, voltages and form factors, Technical article, Texas Instruments, 2020](#)
- [4] [Selecting a Bidirectional Converter Control Scheme, Texas Instruments, 2017](#)
- [5] [100-A, Dual-Phase Digital Control Battery Tester Reference Design, Texas Instruments, 2023](#)



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